

RESEARCH MEMORANDUM

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SOME RECENT DATA FROM FLIGHT TESTS

OF ROCKET-POWERED MODELS

By Langley Pilotless Aircraft Research Division

Langley Aeronautical Laboratory
Langley Field, Va.

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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

WASHINGTON

February 7, 1951





NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

RESEARCH MEMORANDUM

SOME RECENT DATA FROM FLIGHT TESTS

OF ROCKET-POWERED MODELS

By Langley Pilotless Aircraft Research Division

A survey has been made of recent flight data from rocket-powered models which are thought to be particularly applicable to the current U. S. Air Force interceptor competition and which are not yet available in the usual report form. These data are presented herein along with some recently published data which are directly applicable. The data are presented with no discussion or analysis. Some of the data have been taken from investigations that are still incomplete. Proper analysis and discussion will be made in forthcoming NACA papers.

The attached table presents a listing of the subjects covered, the configurations for which data are presented, and references to the figures containing model drawings and data for each configuration.

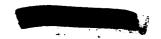
Langley Aeronautical Laboratory
National Advisory Committee for Aeronautics
Langley Air Force Base, Va.



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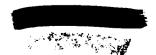
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- 3. Mitcham, Grady L., Stevens, Joseph E., and Norris, Harry P.:
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- 7. Gillis, Clarence L.: Buffeting Information Obtained from Rocket-Propelled Airplane Models Having Thin Unswept Wings. NACA RM L50H22a, 1950.
- 8. D'Aiutolo, Charles T., and Mason, Homer P.: Preliminary Results of the Flight Investigation between Mach Numbers of 0.80 and 1.36 of a Rocket-Powered Model of a Supersonic Airplane Configuration Having a Tapered Wing with Circular-Arc Sections and 40° Sweepback.

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- 10. Baals, Donald D., Smith, Norman F., and Wright, John B.: The Development and Application of High-Critical-Speed Nose Inlets. NACA Rep. 920, 1948.
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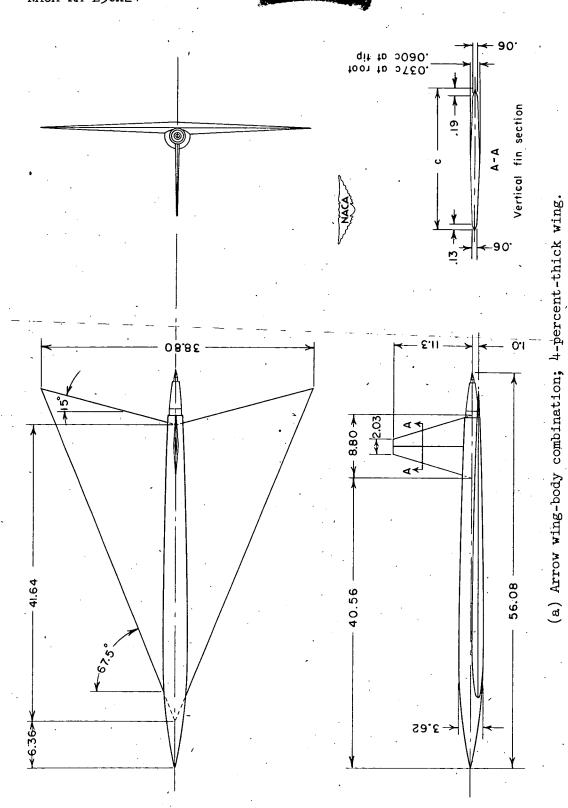




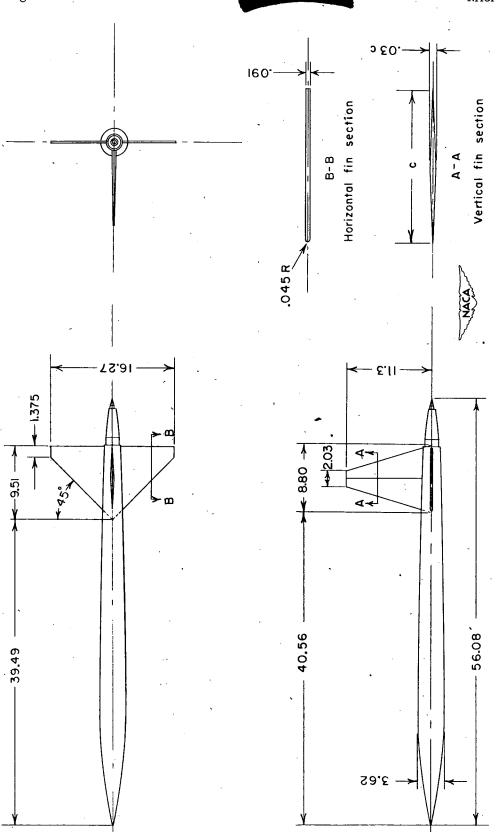
TABLE

		•	
	W-2-1	Figure 1	numbers
'Item	Model	Configurations	Data
Wing drag: (1) Zero-lift drag (Reynolds No. 10 to 50×10^6)			
(a) 3, 4, and 6-percent-thick delta wings (b) 6-percent-thick 45° swept wing (two different bodies)	1, 5, 6, 7 3, 4	1, 3 3	2, 4, 8, 9, 10 4, 6, 7
(c) 4.5-percent-thick straight wing (2) Drag due to lift	2 5	3	4, 5
(a) 6.5-percent-thick delta trimmed with	8	11	17
elevator (b) 6.5-percent-thick delta trimmed with canard surfaces	9	12	17
(c) 40° and 60° swept wings (d) 4.5-percent-thick straight wings	10, 11 12	13, 14 15	18, 19 19
Body drag: (1) Drag of radome noses (2) Drag of canopies	13 14	20 21	.20 22
Inlet drag and pressure recovery: (1) Sharpened-lip nose inlet and basic body (2) Subsonic nose inlet and basic body	15, 16 15, 17	- 23 23	24, 25 26, 27
Lift characteristics: (1) 6.5-percent-thick delta wings, tailless and with canard	8, 9	11, 12	28
(2) 40°, 42°, and 60° swept wings with tail (3) 4.5-percent-thick straight wing with tail	10, 11, 18	13, 14, 16 15	. 28 28
Aerodynamic-center location: (1) 6.5-percent-thick delta wings, tailless and with canard	8, 9	11, 12	29
(2) 40°, 42°, and 60° swept wings with tail (3) 4.5-percent-thick straight wing with tail	10, 11, 18	13, 14, 16 15 [.]	29 29
Longitudinal control: (1) 6.5-percent-thick delta wings with elevator (tailless) and with canard	8,9	11, 12	30 ·
(2) 40° swept wing with elevator (3) 4.5-percent-thick straight wing with all-movable tail	10 12	13 15	30 . 30
Longitudinal damping: (1) 6.5-percent-thick delta wings, tailless and with canard	8,9	11, 12	31
(2) 40°, 42°, and 60° swept wings with tail (3) 4.5-percent-thick straight wing with tail	10, 11, 18	13, 14, 16 15	31 31
Damping in roll: (1) 6-percent-thick 45°, 60°, and 70° delta wings (2) 35°, 40°, 45°, and 63° swept wings	20, 21, 22	32, 33 32, 34, 35, 36	33 34, 35, 36
(3) 4.5 and 6-percent-thick straight wings	23, 24 25, 26	37	37

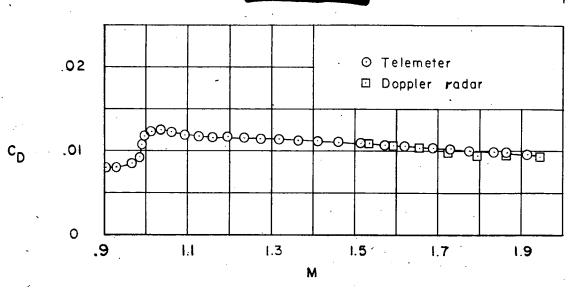


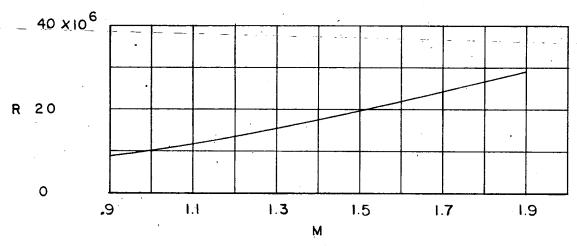


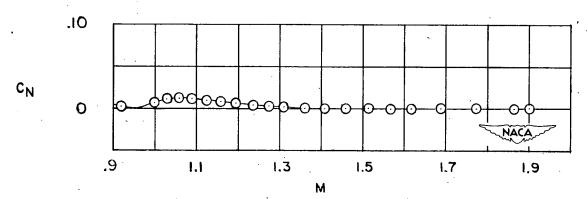
All dimensions are in inches. Figure 1. General arrangement of model 1.



(b) Wingless model.
Figure 1.- Concluded.



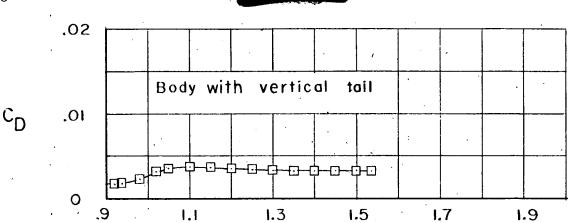




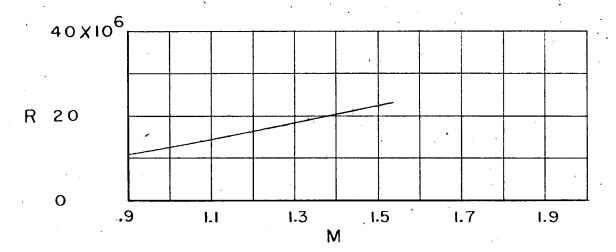
(a) CD, R, and CN against M for arrow wing-body model.

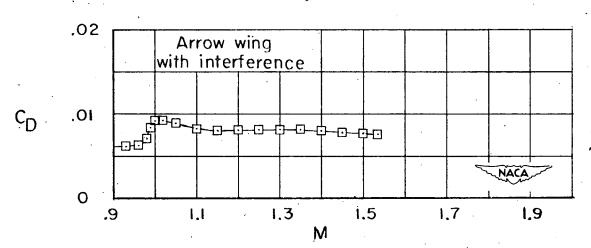
Figure 2.- Data from coasting flight of model 1. C_{D} based on total wing to fuselage center line.





M





(b) C_{D} and R against M from wingless model. Figure 2.- Concluded.



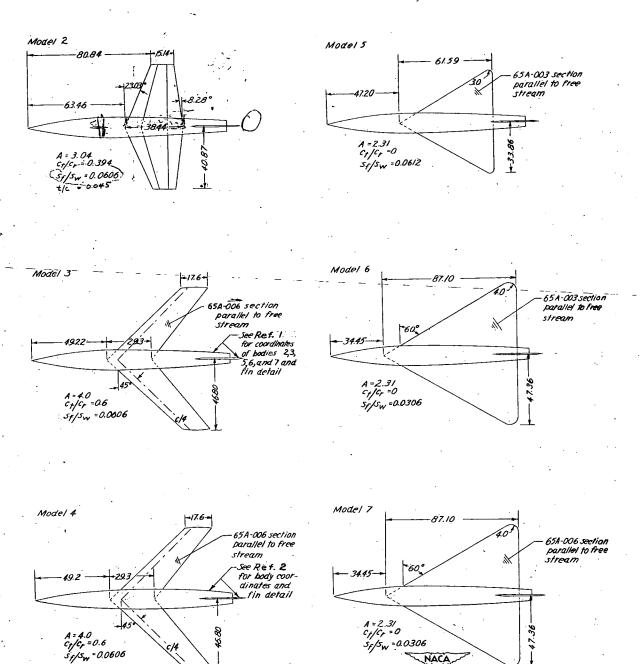


Figure 3.- Plan forms of models 2, 3, 4, 5, 6, and 7. (All dimensions are in inches.)

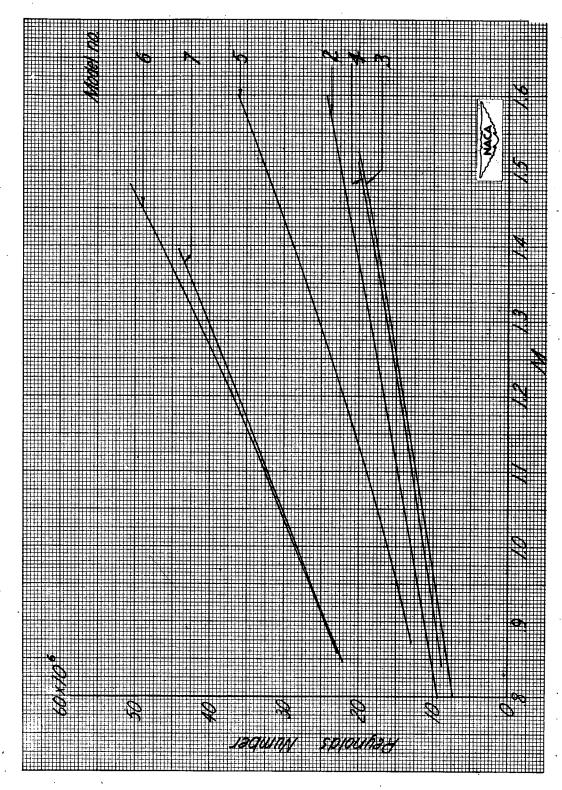
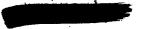
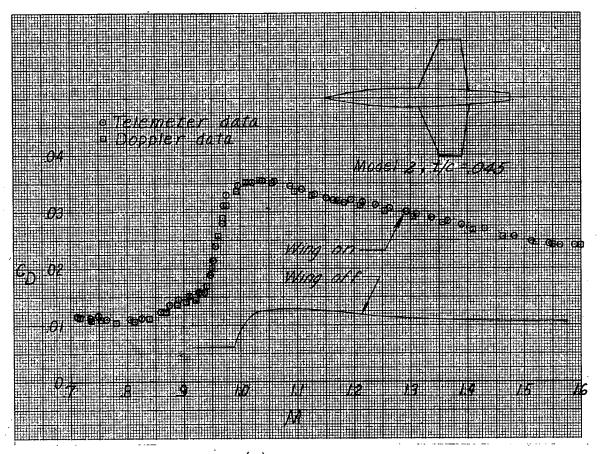


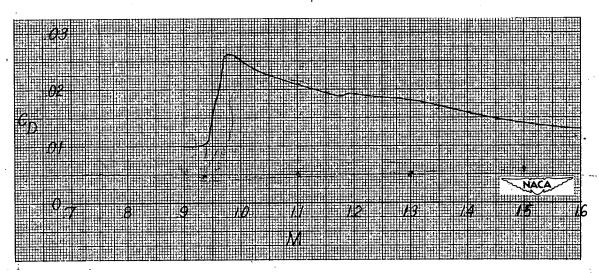
Figure μ . Variation of Reynolds number with Mach number for the wing-body configuration, based on wing mean aerodynamic chord.







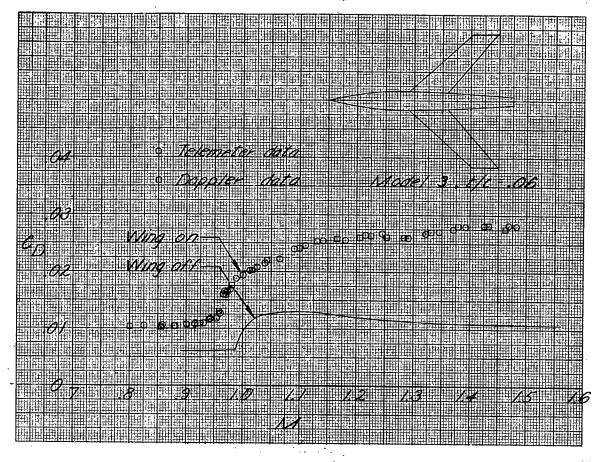
(a) Total drag.



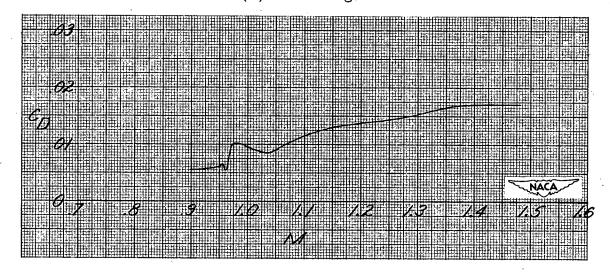
(b) Wing-plus-interference drag.

Figure 5.- Drag of a straight wing on a parabolic body, model 2. $C_{\rm D}$ based on total wing to fuselage center line.



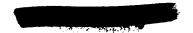


(a) Total drag.

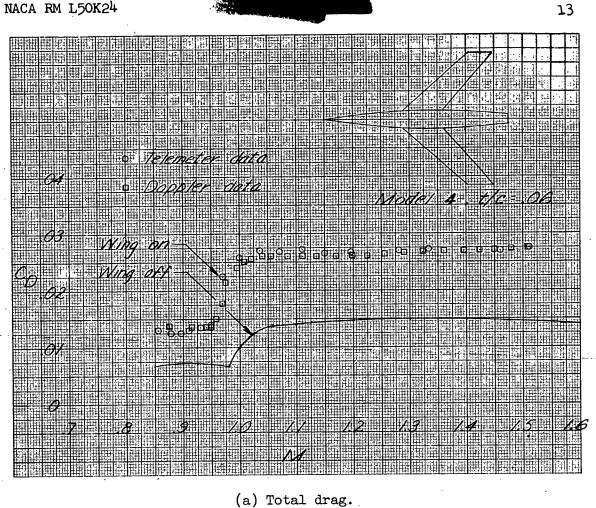


(b) Wing-plus-interference.

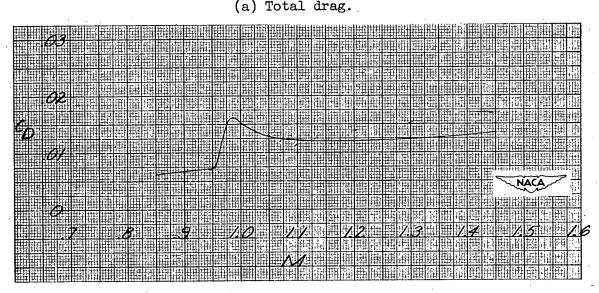
Figure 6.- Drag of a 45° swept wing on a parabolic body, model 3. $c_{\rm D}$ based on total wing to fuselage center line.







(a) Total drag.

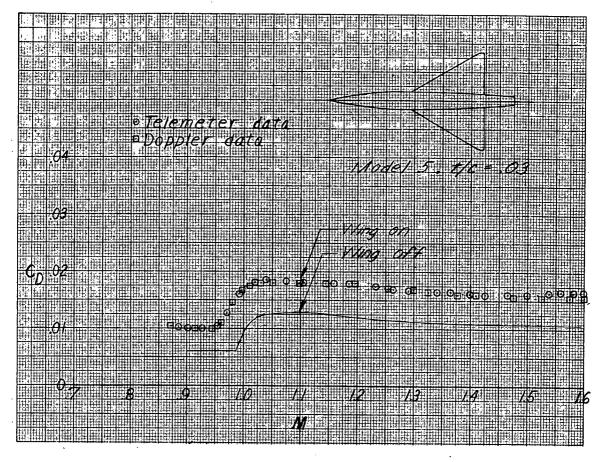


(b) Wing-plus-interference drag.

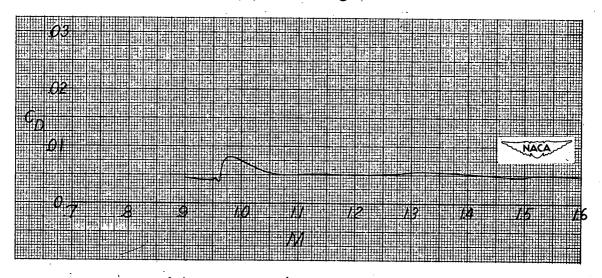
Figure 7.- Drag of a 45° swept wing on a transonic body, model 4. reference 2.) CD based on total wing to fuselage center line.





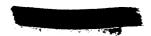


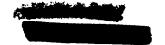
(a) Total drag.

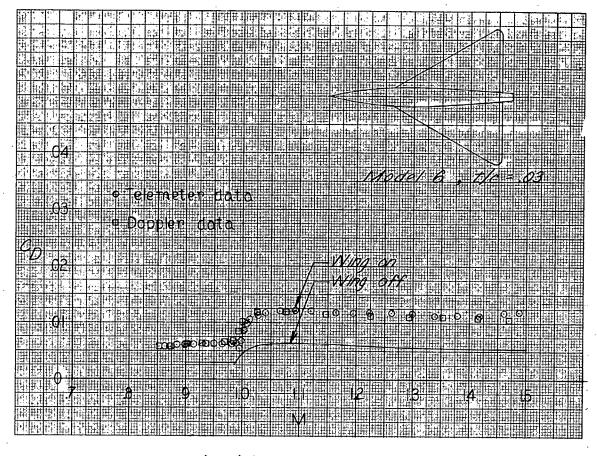


(b) Wing-plus-interference drag.

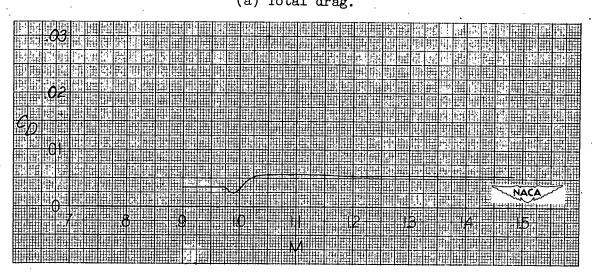
Figure 8.- Drag of a small 60° delta wing on a parabolic body, model 5. (See reference 1.) $C_{\rm D}$ based on total wing to fuselage center line.







(a) Total drag.

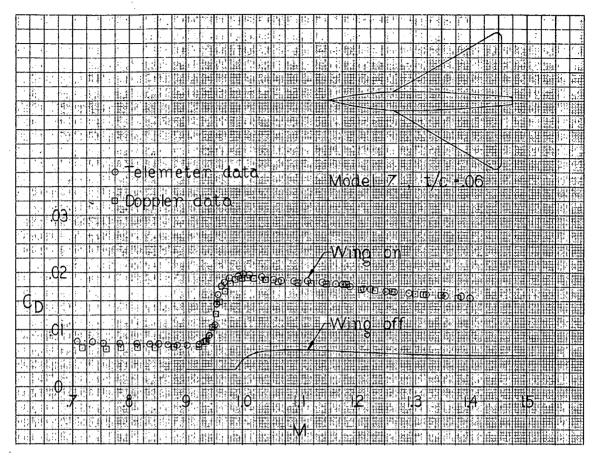


(b) Wing-plus-interference drag.

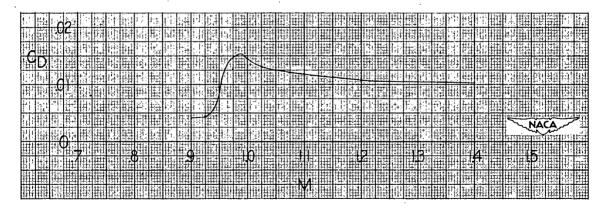
Figure 9.- Drag of a large 60° delta wing on a parabolic body, model 6. (See reference 1.) c_D based on total wing to fuselage center line.







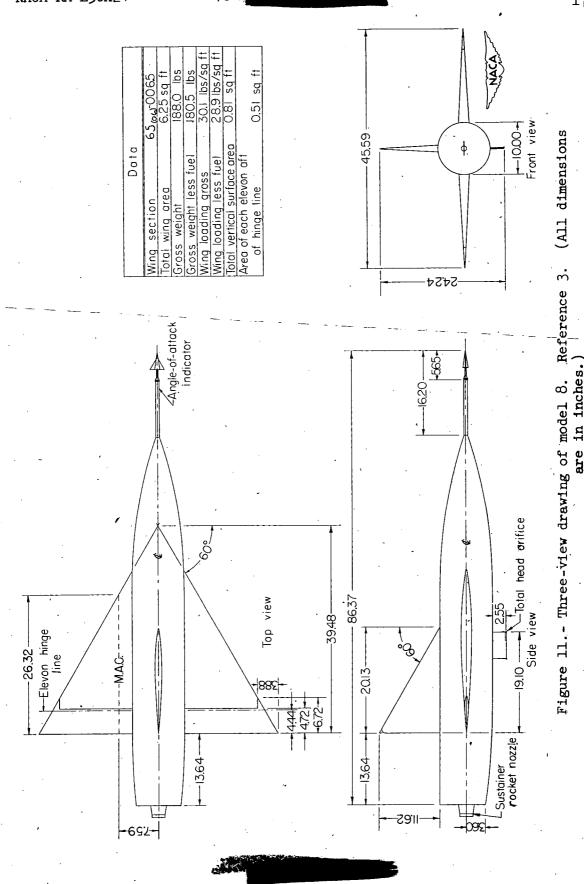
(a) Total drag.



(b) Wing-plus-interference drag.

Figure 10.- Drag of a large 60° delta wing on a parabolic body, model 7. $C_{\rm D}$ based on total wing to fuselage center line.





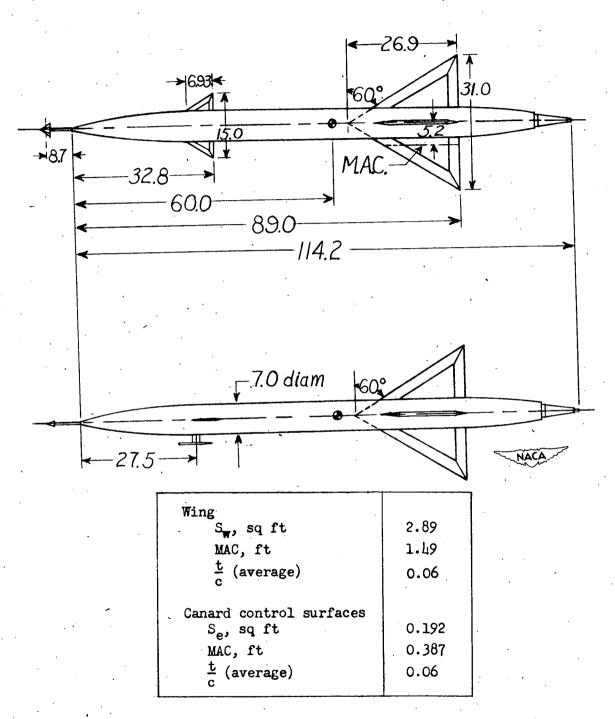


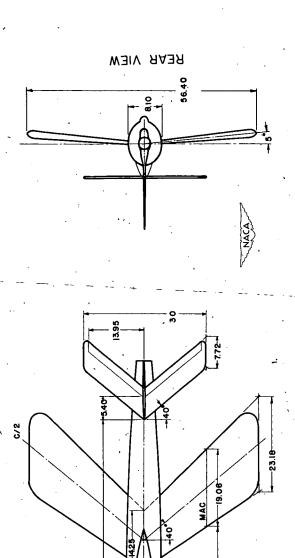
Figure 12.- General arrangement of model 9. All dimensions in inches.

Reference 4.





TOP VIEW



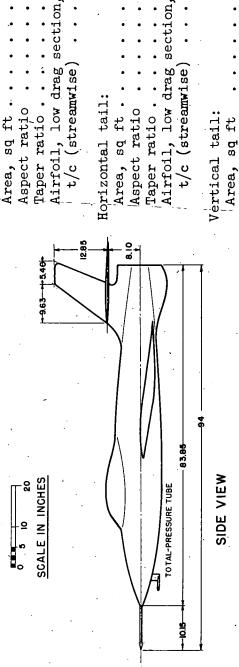
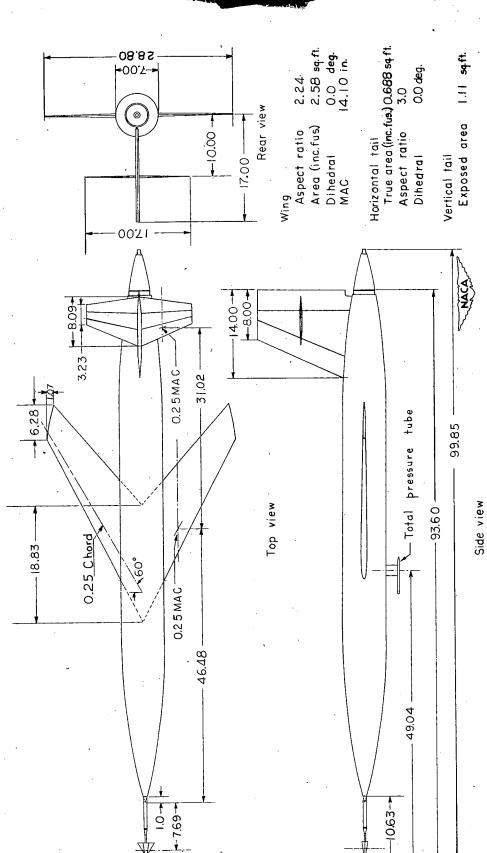
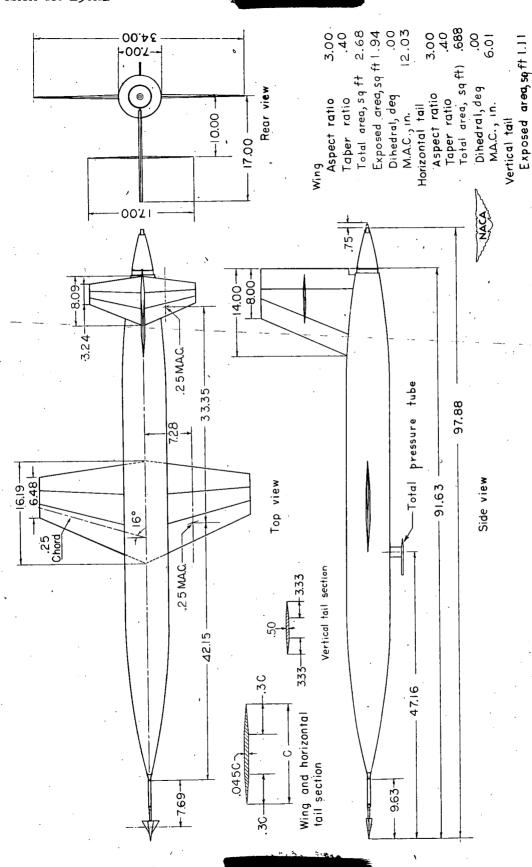


Figure 13.- General arrangement of model 10. (See reference 5.)



 $\frac{t}{c} = 0.049$ streamwise at Figure 14. - General arrangement of model 11. Wing of 64-series airfoll; $\frac{t}{c} = 0.063$ streamwise at wing-body juncture; tip. (All dimensions are in inches.)



(See references 6 and 7.) (All dimensions are in inches. Figure 15. - General arrangement of model 12.

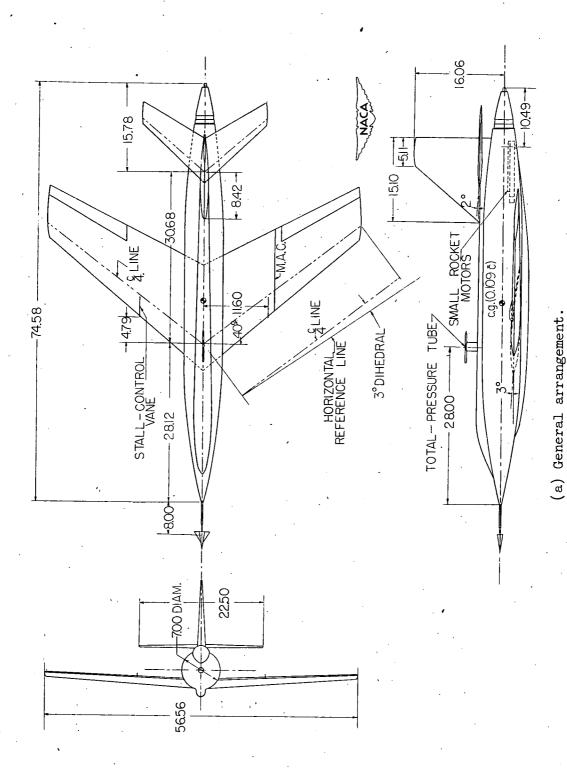
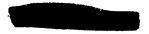
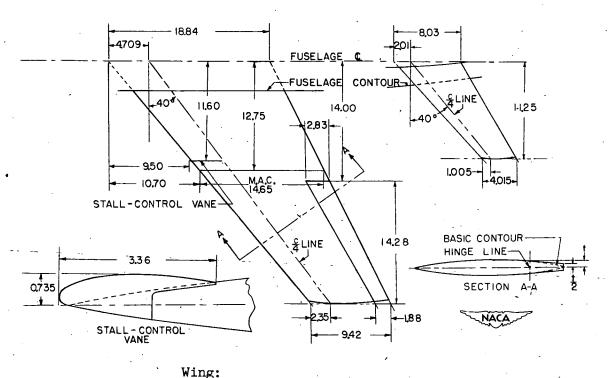


Figure 16.- Model 18 (reference 8).





ing:								
Area, sq ft .	•	•						5.56
Aspect ratio							•	4.00
Taper ratio .		•					•	0.50
Airfoil section	on,	r	101	rma	al			
to c/4 line,	, c	ii	ci	118	ır.	-a:	rc	,
10 percent t								

Horizontal tail:

Area, sq ft	` • • •	.0.938
Aspect ratio		. 3.72
Taper ratio		. 0.50
Airfoil section, no		-
to $c/4$ line		65-008
•,		

Vertical tail:

Area, sq ft 0.966

(b) Wing and tail details.

Figure 16.- Concluded. Model 18.



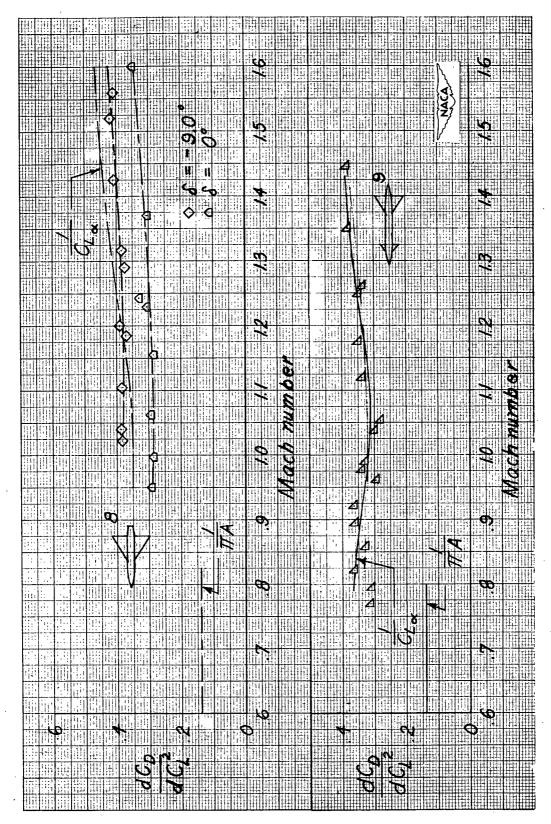


Figure 17.- Drag due to lift of several delta-wing configurations. c_{D} based on total wing area to body center line.



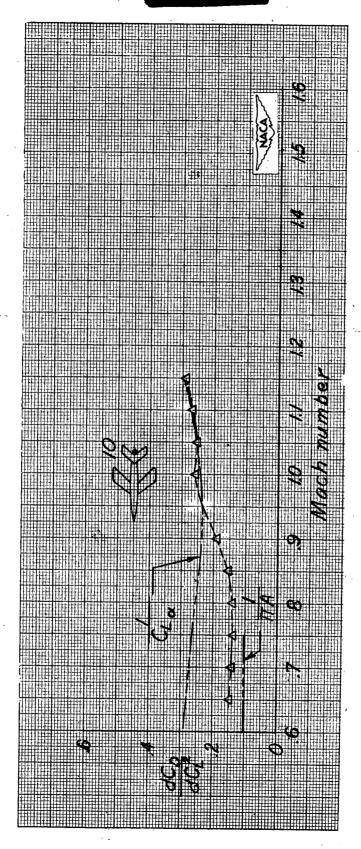


Figure 18.- Drag due to lift of a sweptback-wing configuration. $c_{\rm D}$ based on total wing area to body center line.

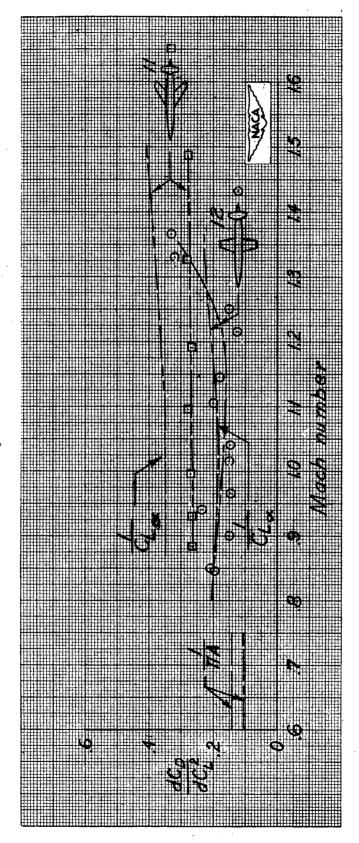
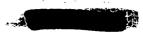
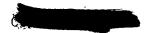


Figure 19.- Drag due to lift of a straight and a sweptback wing with the same fuselage configuration. CD based on total wing area to body center line.





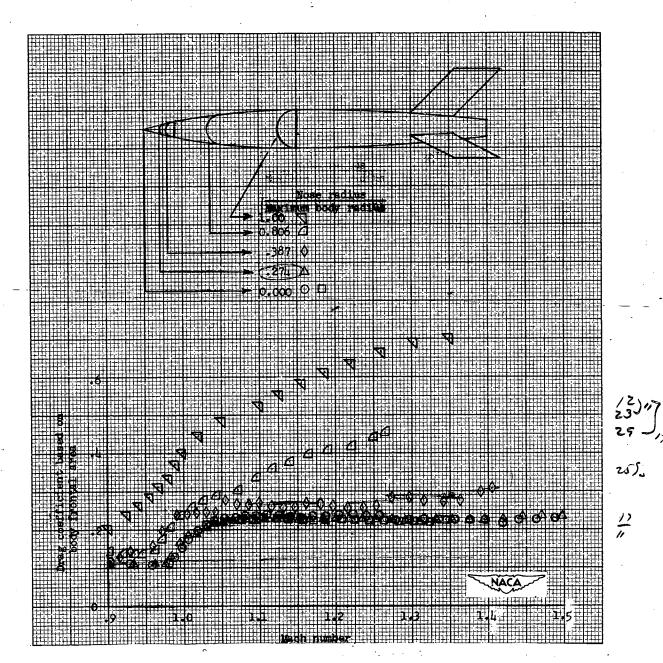
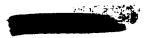
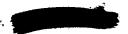
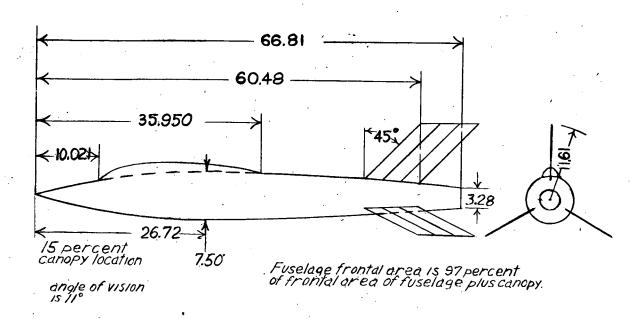
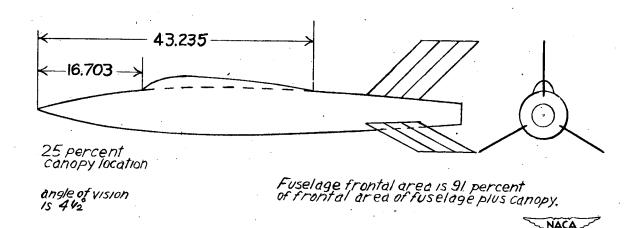


Figure 20.- Drag changes due to rounding off the nose of a fin-stabilized parabolic body of revolution of fineness ratio 8.91. Dimensions of the pointed-nose body may be found in reference 9. Model 13.





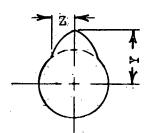




(a) General arrangement.

Figure 21.- Canopies are fineness-ratio-7.82 parabolic bodies (with maximum diameter at 15.5 percent body length) bent to conform to the contour of the fuselage. The fuselage is identical to the parabolic body reported in reference 9. Model 14.





Coordinates
15 percent canopy

Coordinates
25 percent canopy

Fuselage Station	ı Z	Y
10.021	0	2.285
10,500	0.450	2.818
11-000	0_830 -	3.282
12,000	1.365	3.977
14,000	1.705	4.605
16.000	1.781	4.927
18,000	1.640	5.050
20,000	1,560	5.073
22,000	1.455	5.088
24,000	1.344	5.055
26,000	1.182	4.930
28,000	1,000	4.748
30,000	0.805	4.541
32,000	0.560	4.274
34,000	0.285	3.965
35.950	0	3.645

Fuselage Station	Z	Y
16,703	0	3.223
17.000	0.260	3.513
´ 18.000	0.915	4.375
20,000	1.602	5.115
22,000	1,690	5.323
24,000	1,685	5.396
26,000	1,620	5,368
28,000	1.531	5.279
30,000	1.415	5.151
32,000	1,291	5,005
34.000	1.120	4,800
36,000	0,925	4.562
38,000	0.715	4.298
40.000	0.460	3,979
42.000	0,180	3.624
43.235	0	3.392

(b) Coordinates of canopy used. Model 14.

Figure 21.- Concluded.



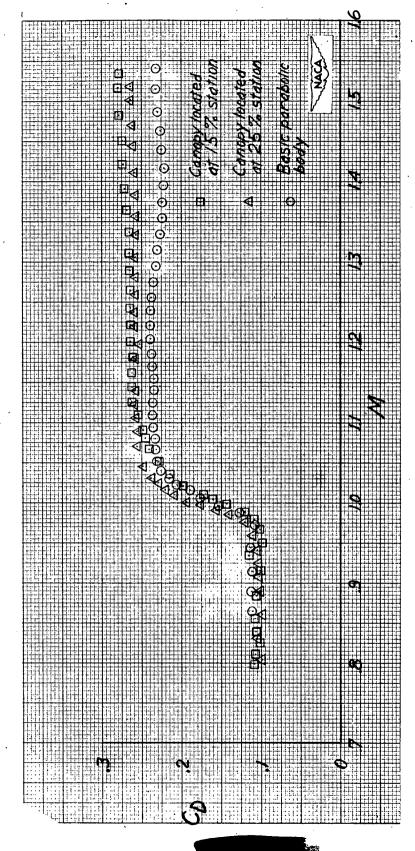


Figure 22. - Total configuration drag coefficient of body-canopy configu- $C_{\rm D}$ based on frontal area of basic body. rations, model 14.

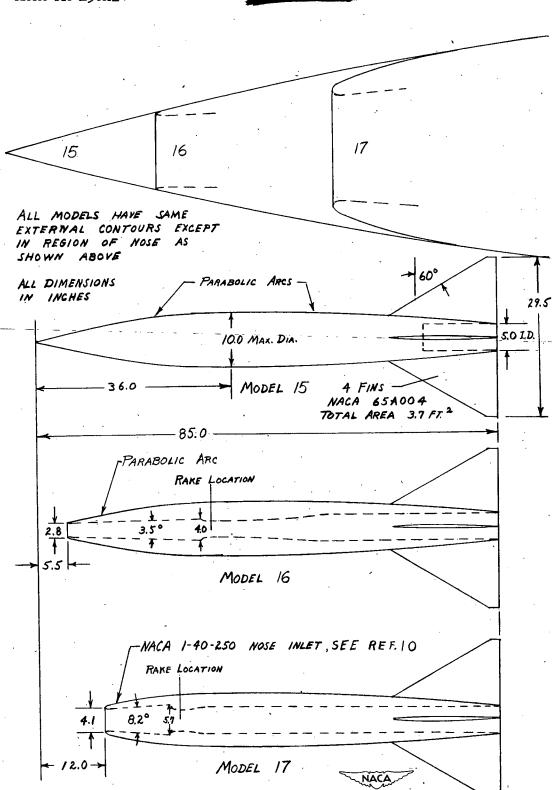
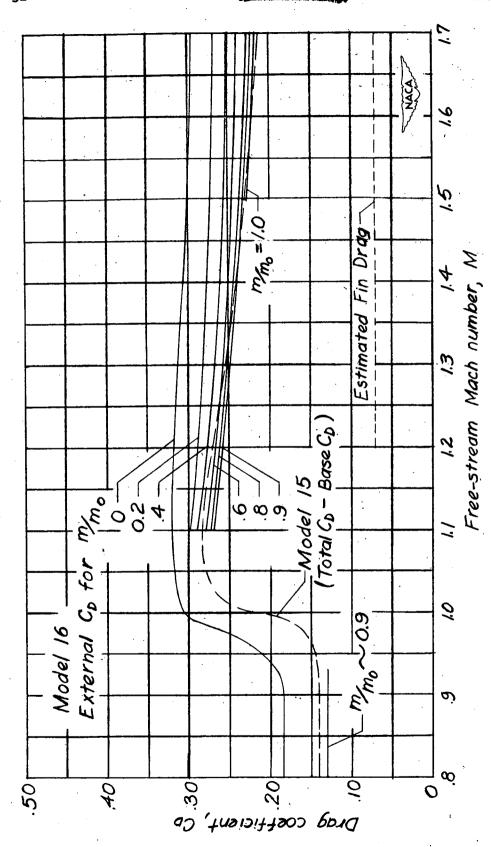
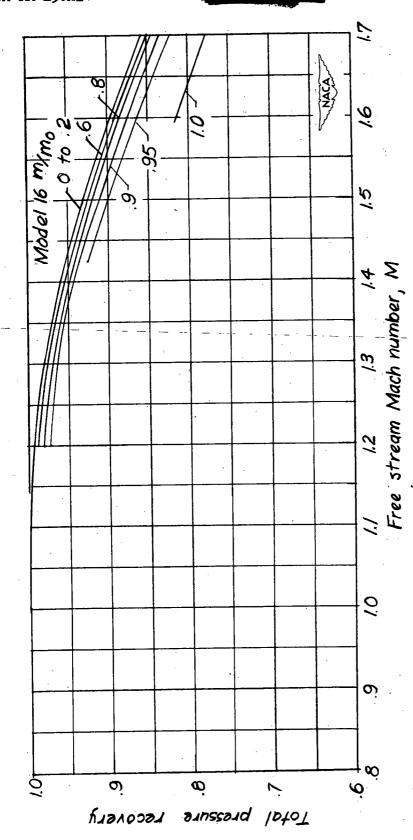


Figure 23. General arrangement of models 15, 16, and 17.



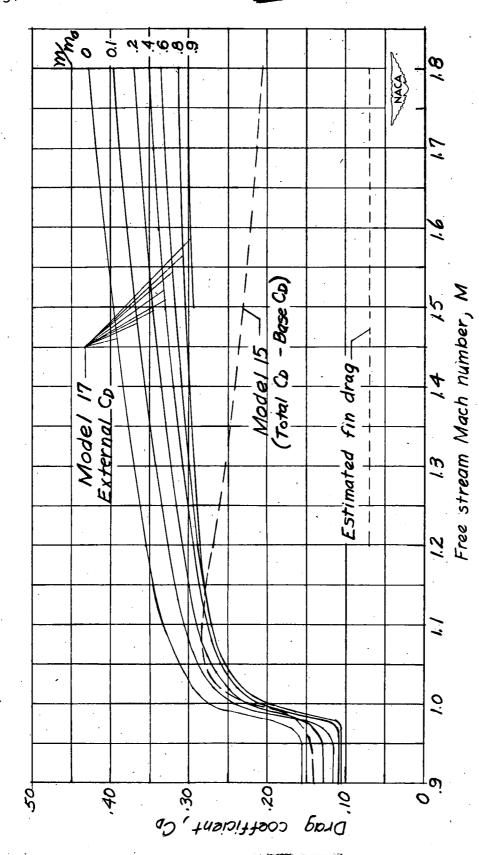


several mass-flow ratios for model 16. CD based on body frontal area. Figure 24. Variation of external drag coefficient with Mach number for still being reduced.) (Data for medium flow rates at M < 1.1



(Data for lower Mach numbers Figure 25.- Variation of total-pressure recovery with Mach number for several mass-flow ratios for model 16. still being reduced.)





based on body frontal area. Figure 26.- Variation of external drag coefficient with Mach number for c_D several mass-flow ratios for model 17.

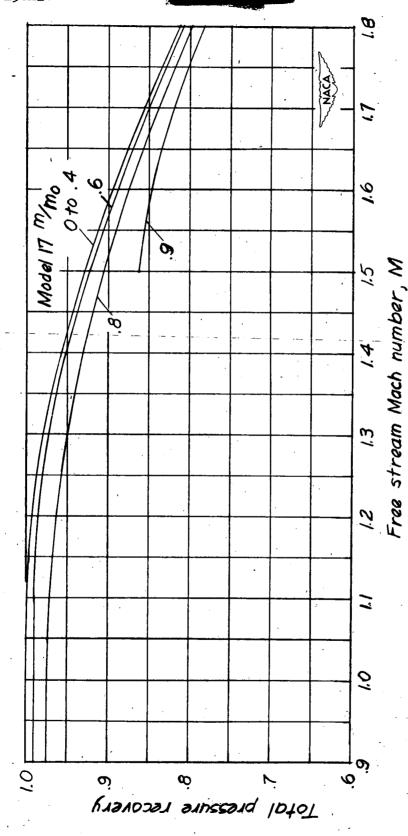


Figure 27. - Variation of total pressure recovery with Mach number for several mass-flow ratios for model 17.





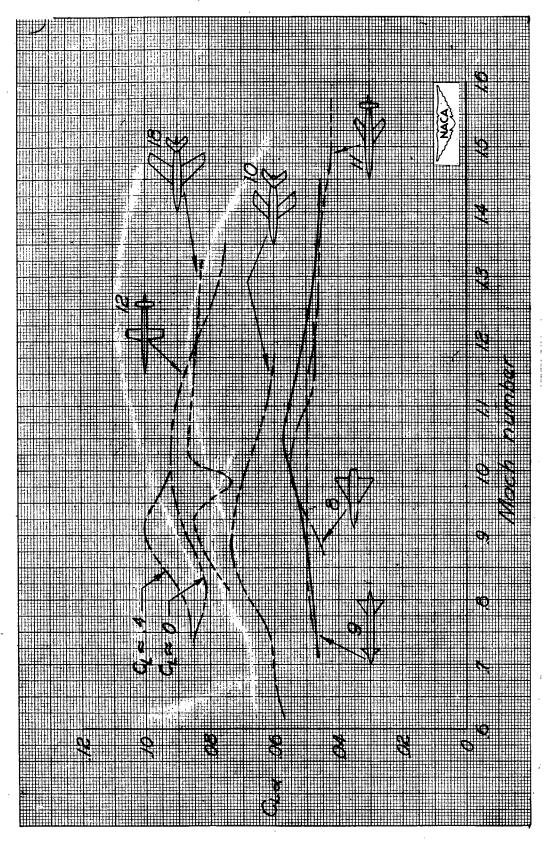


Figure 28.- Lift-curve slopes of various configurations. c_{L} total wing area to body center line.

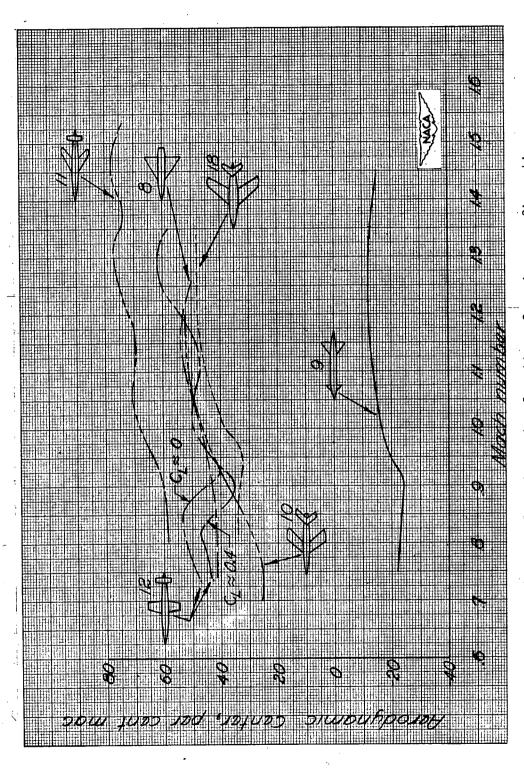
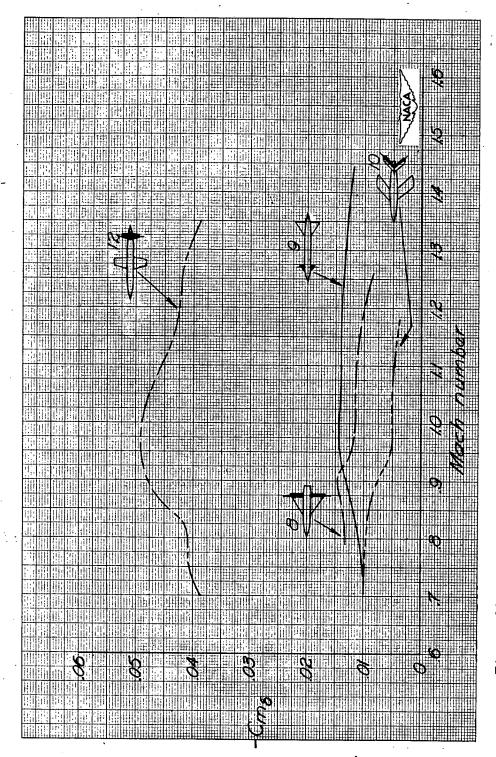


Figure 29. - Aerodynamic-center location of various configurations







pitching moment for various configurations, based on wing dimensions to body center line. Figure 30. - Effectiveness of the longitudinal control in producing



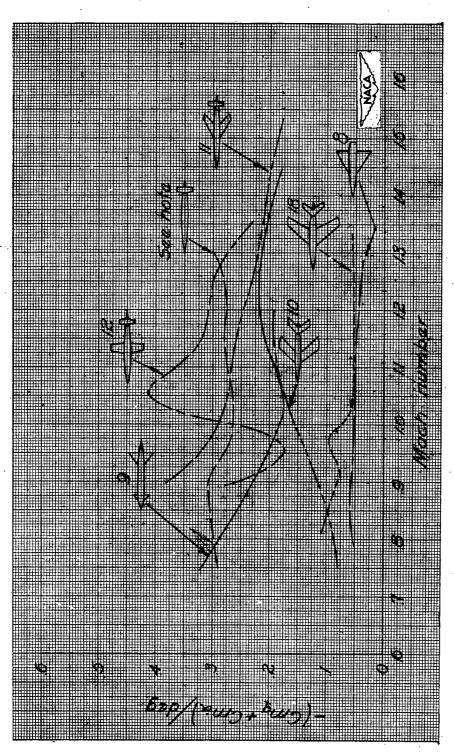
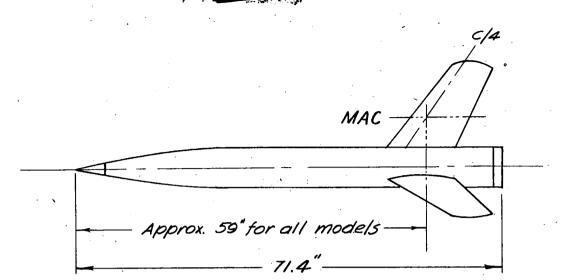


Figure 31.- Total damping-in-pitch derivative of various configurations. Note: Data for body and tail of models 11 and 12 based on wing dimensions of model 12.



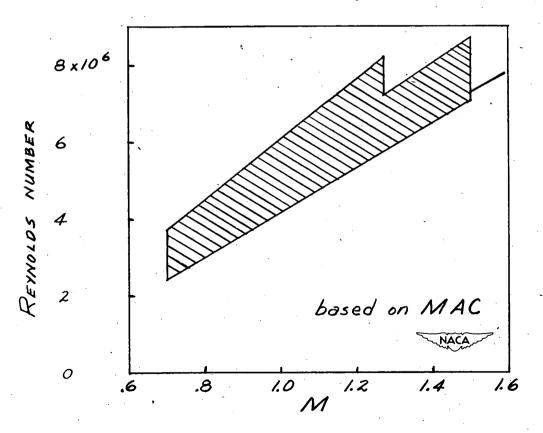
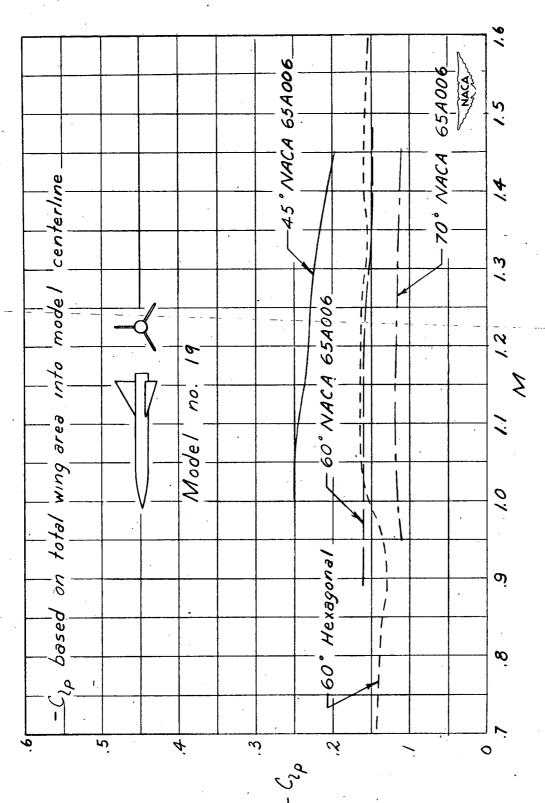


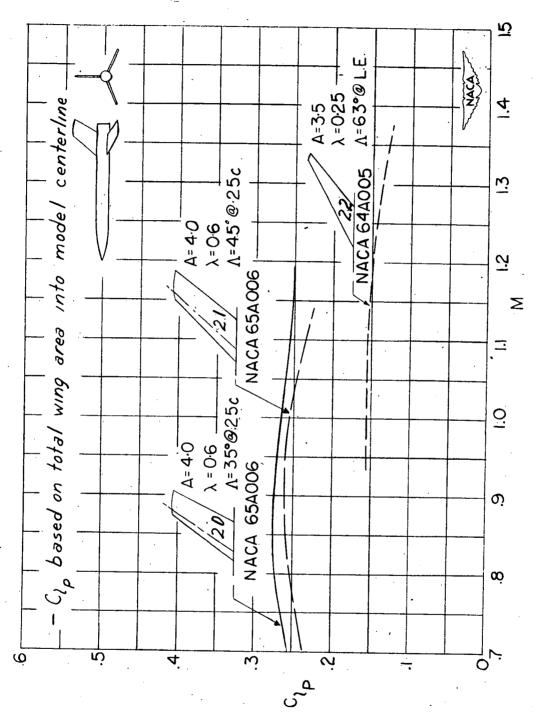
Figure 32.- Damping-in-roll model and scale of tests. Reference 11.



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Figure 33.- Damping in roll of a series of triangular wings. sections parallel to model center line.





Airfoil sections Figure 34.- Damping in roll of swept tapered wings. parallel to model center line.



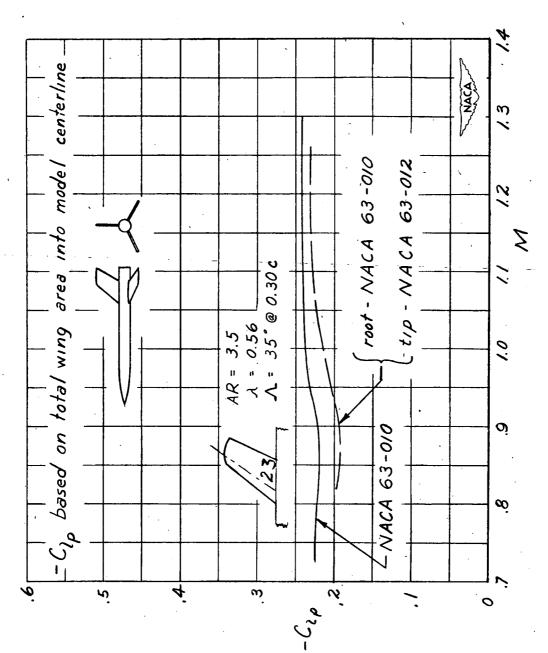


Figure 35.- Damping in roll of a swept wing with two thickness ratios. Airfoil section parallel to model center line.

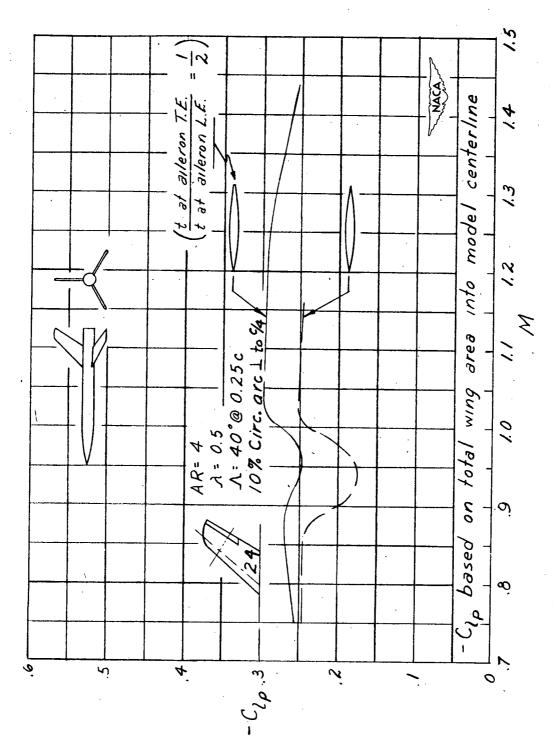
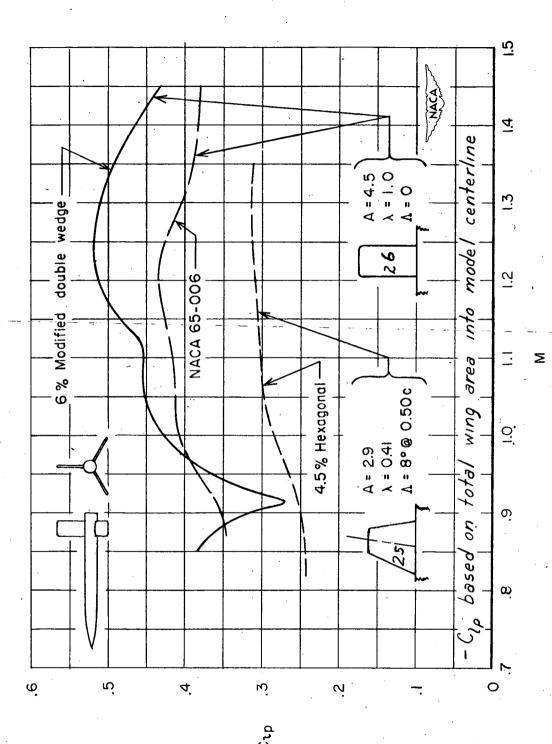


Figure 36.- Damping in roll of a swept wing with modified trailing edge.



Airfoil sections Figure 37.- Damping in roll of essentially unswept wings. parallel to model center line.